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(54) **SYSTEMS AND METHODS TO PROVIDE
COMPENSATED FEEDBACK PHASE
INFORMATION**

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H04L 27/36 (2006.01)

(52) **U.S. Cl.**
CPC **H03C 5/00** (2013.01); **H04L 27/361**
(2013.01); **H04L 27/368** (2013.01)

(58) **Field of Classification Search**
USPC 375/295, 296, 297, 300, 302, 308
See application file for complete search history.

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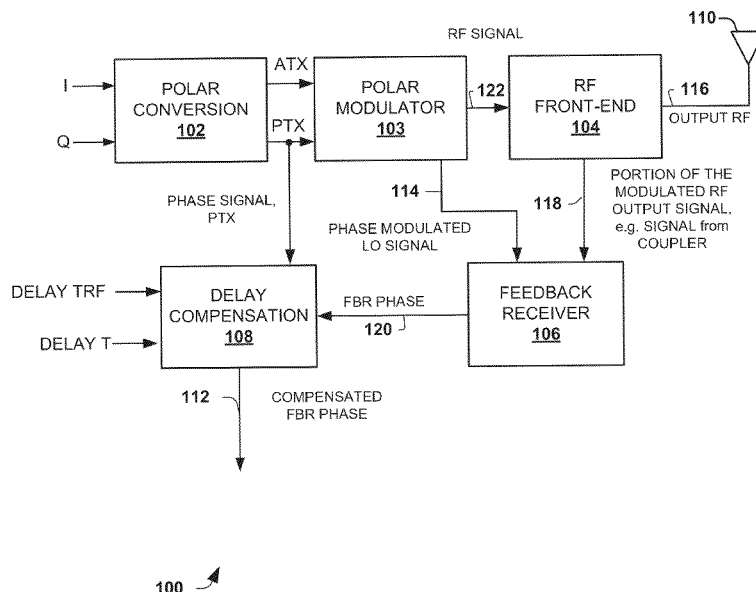
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(57) **ABSTRACT**

A communication system includes a polar conversion component, a polar modulator, an RF front-end component, a feedback receiver, a delay compensation component, and an adder. The polar conversion component is configured to provide an amplitude signal and a phase signal. The polar modulator is configured to receive amplitude signal and the phase signal and to provide the phase modulated local oscillator signal and an RF output signal. The RF front-end component is configured to receive the RF output signal and to provide a coupled output signal. The feedback receiver is configured to receive the phase modulated local oscillator signal and the coupled output signal and to generate an uncompensated feedback phase information signal. The delay compensation component is configured to receive the phase signal and the uncompensated feedback phase information signal and to generate a compensation signal. The adder is configured to add the compensation signal to the uncompensated feedback phase information signal to generate a compensated feedback phase information signal.

17 Claims, 9 Drawing Sheets



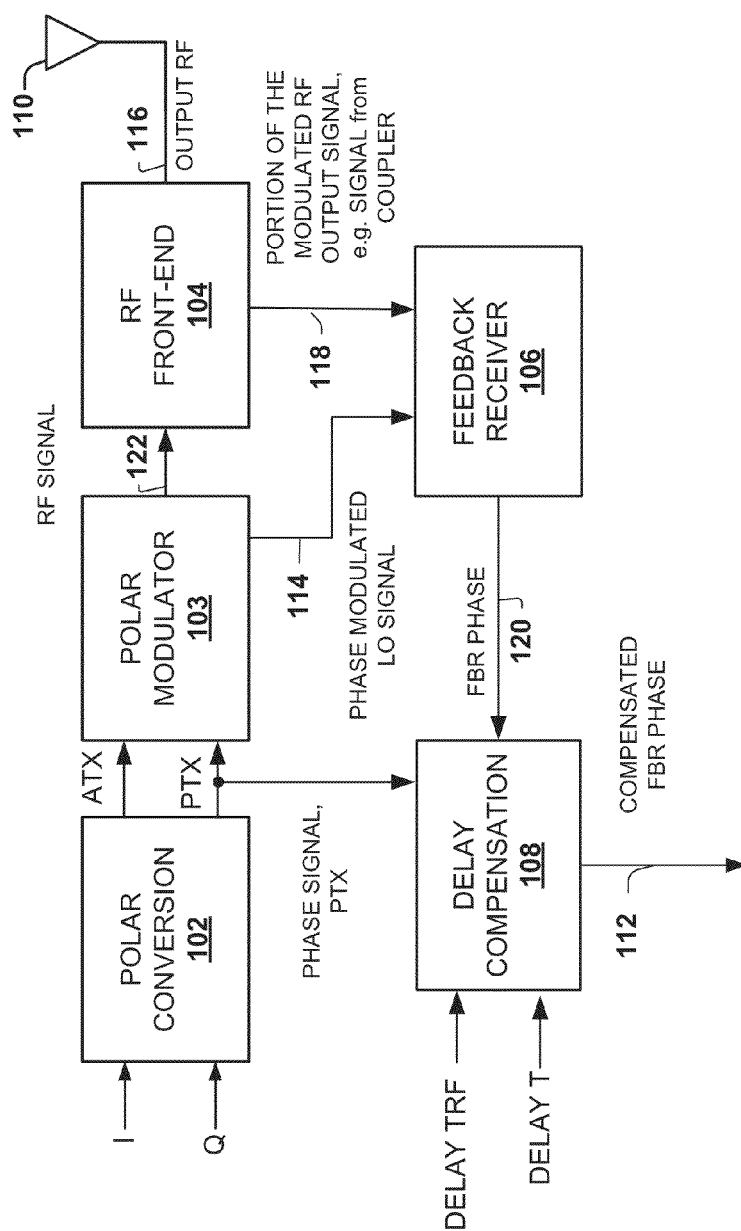


FIG. 1

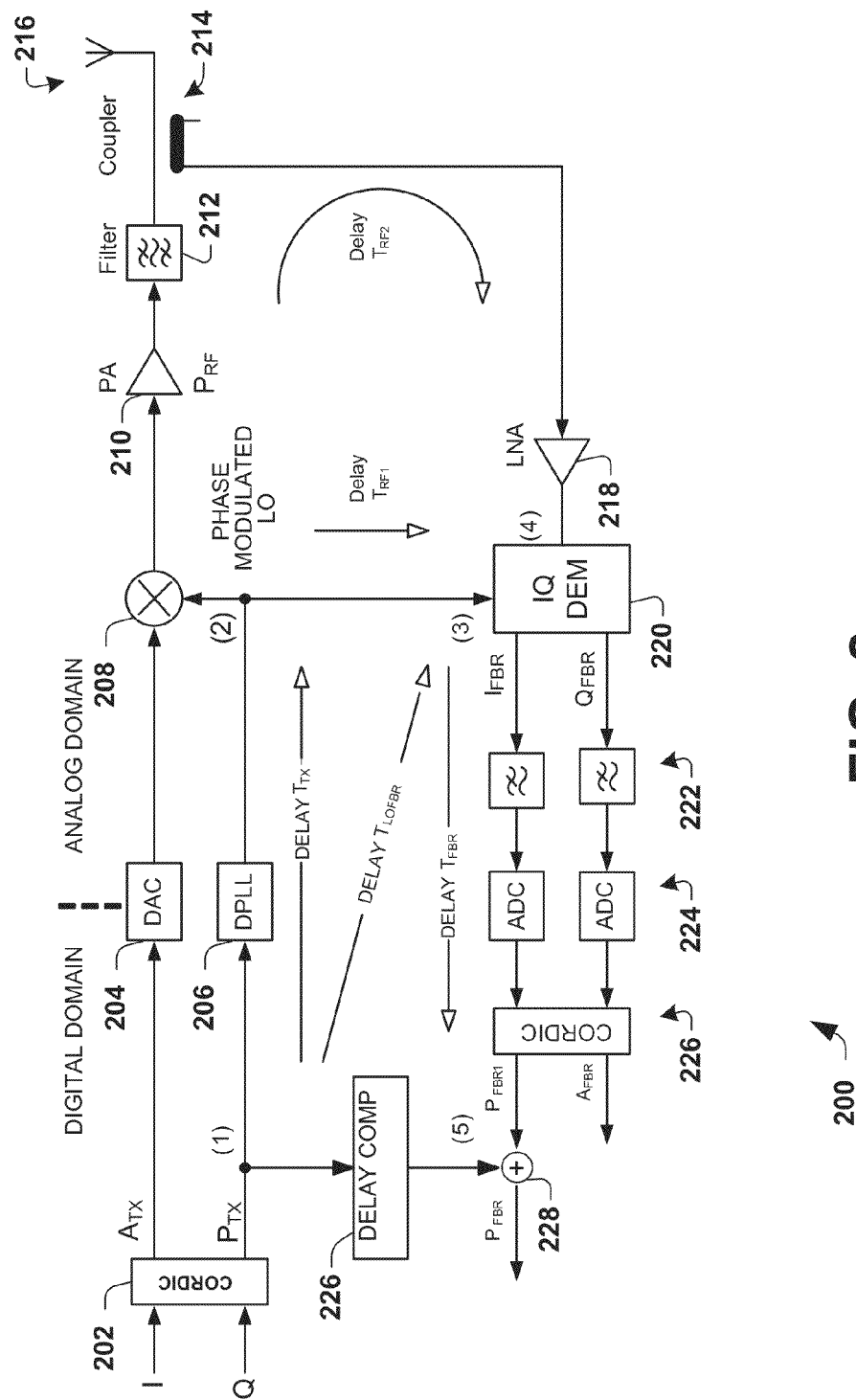


FIG. 2

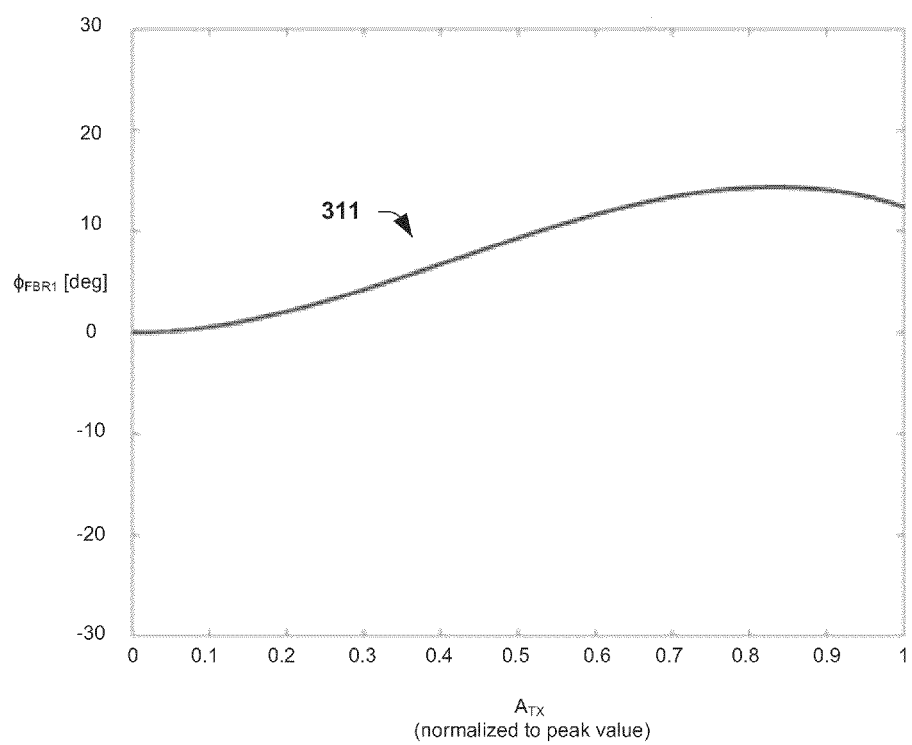
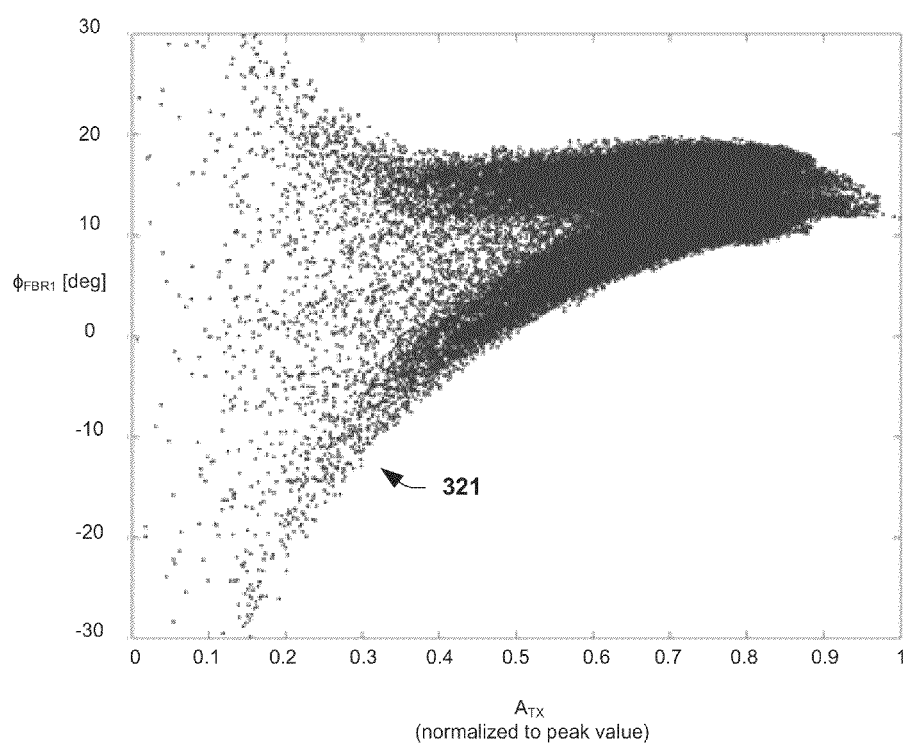


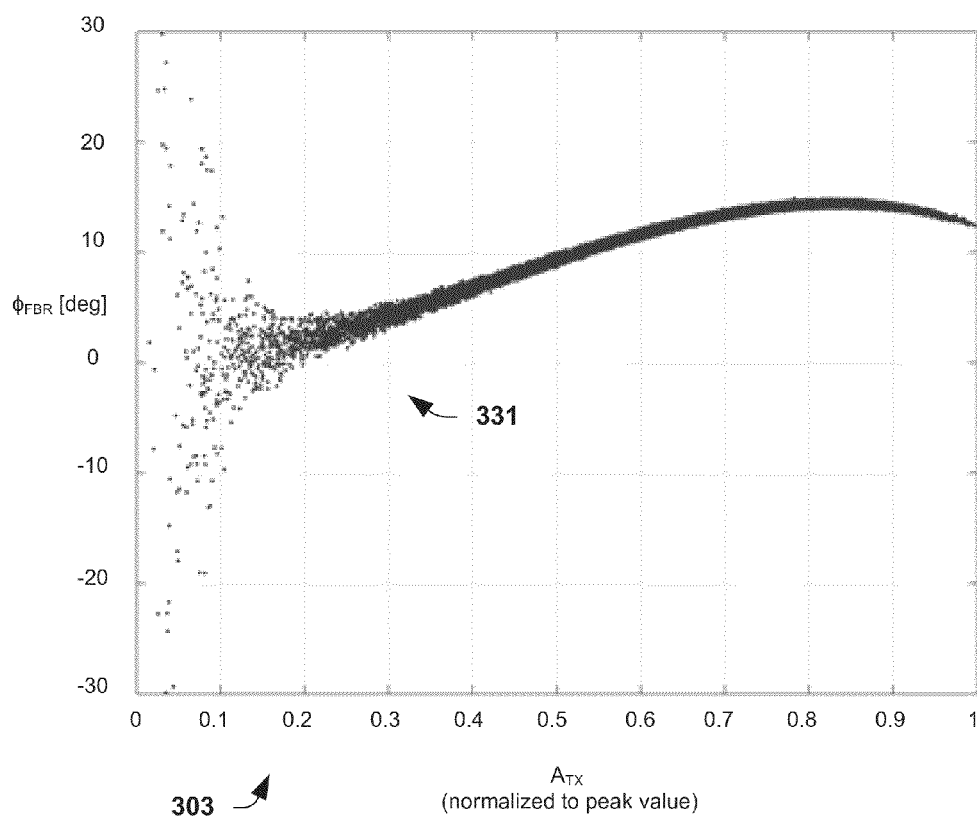
FIG. 3A

301



302

FIG. 3B

**FIG. 3C**

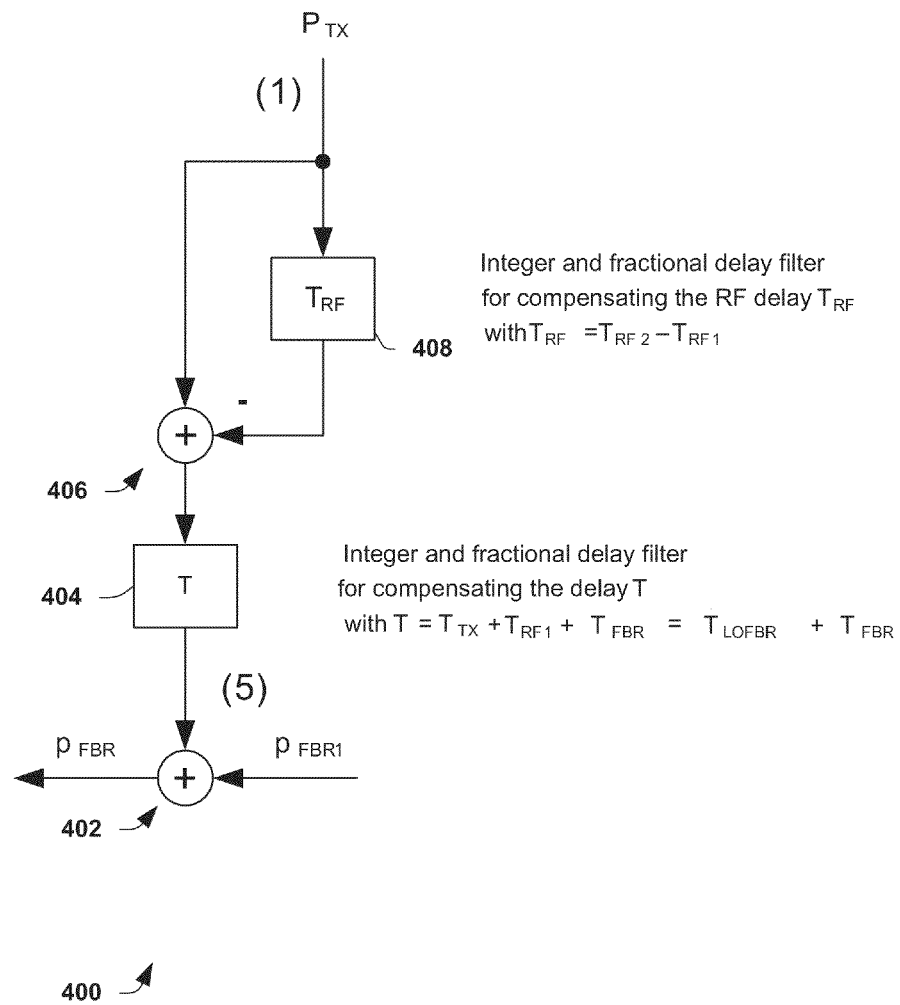


FIG. 4

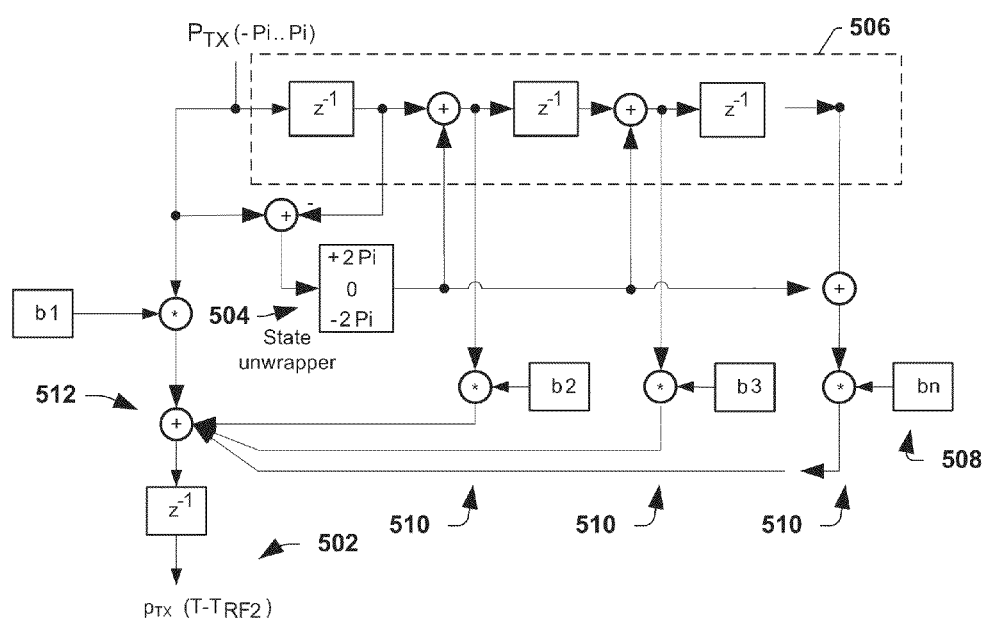


FIG. 5


```
filterorder=1

for m=0:filterorder
    for k=0:filterorder
        if k~=m
            M1(k+1)=(Delay-k)/(m-k);
        else
            M1(k+1)=1;
        end
    end
    b(m+1)=prod(M1);
    clear M1;
end
```

600 

FIG. 6

```
if ((phase(i1)-phase(i1-1))>1.5*pi)
    buffer=(phase(i1-1)+2*pi);
elseif((phase(i1)-phase(i1-1))<-1.5*pi)
    buffer=(phase(i1-1)-2*pi);
else
    buffer=phase(i1-1);
end

delayed_phase(i1)=phase(i1)*b(1)+buffer*b(2);
```


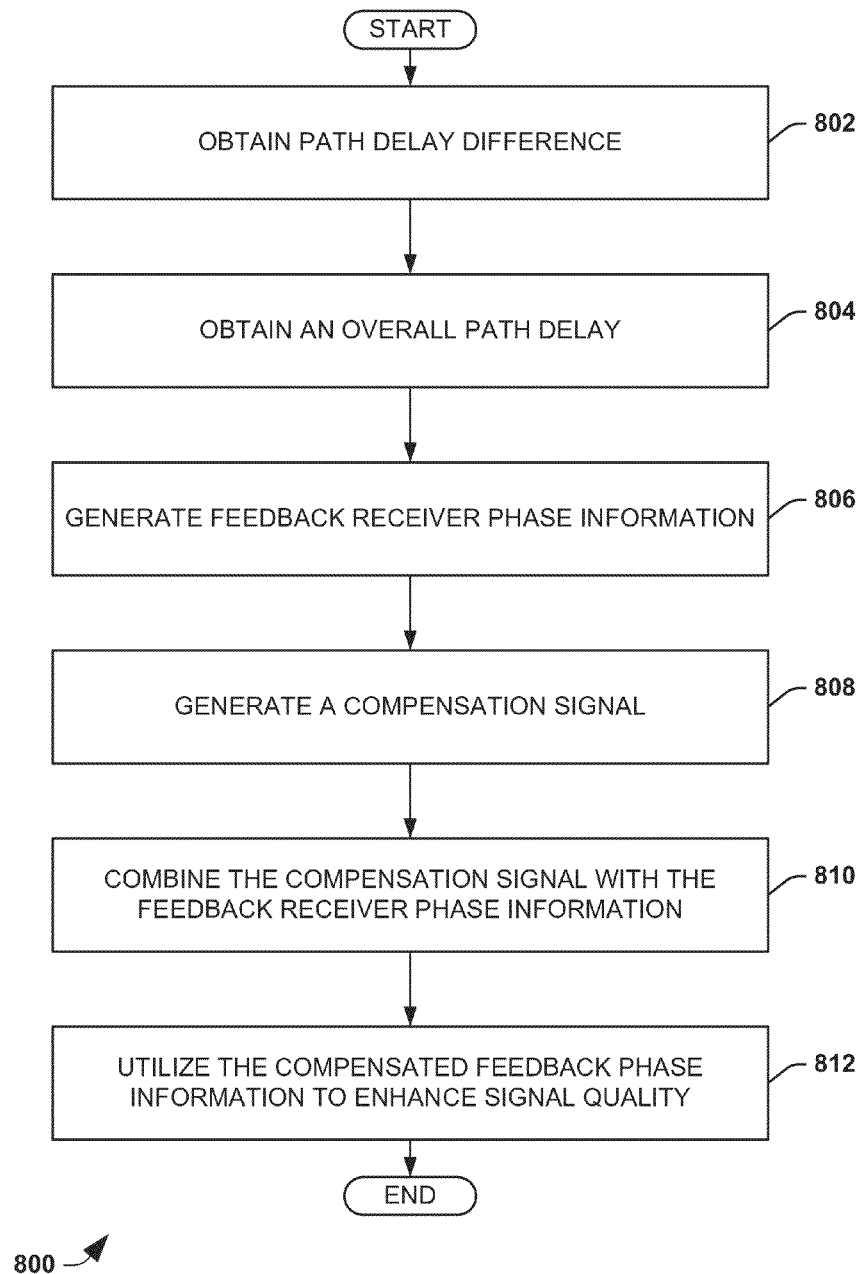
700 

FIG. 7

**FIG. 8**

SYSTEMS AND METHODS TO PROVIDE COMPENSATED FEEDBACK PHASE INFORMATION

BACKGROUND

Traditional designs of RF-modulator in wireless communication systems like LTE, HSPA, Bluetooth, WLAN, GSM-EDGE, and the like, employ vector modulator architectures which operate essentially as a single-sideband up-converter (SSB) using two digital-to-analog converters (DAC), two mixers and a power amplifier (PA). A different concept, the polar modulator concept separates the modulation signal into an amplitude modulation (AM) signal and a phase modulation (PM) signal. The symbols or points used in polar modulation correspond or translate from Cartesian coordinates utilized in vector modulation concepts. An additional feedback receiver (FBR) connected to the output of the transmitter can be useful for output power control, digital pre-distortion (DPD) and impedance matching. The usage of the phase modulated local oscillator (LO) signal also for the down conversion in the feedback receiver can utilize the measurements of the output amplitude and the phase shift of the PA.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a simplified diagram illustrating a communication system **100** employing polar modulation.

FIG. 2 is a diagram illustrating a communication system employing polar modulation.

FIG. 3A is a graph illustrating the FBR phase information from a feedback receiver with phase modulated LO for the ideal case where the RF delay T_{RF} is zero.

FIG. 3B is a graph illustrating the FBR phase information from a feedback receiver with phase modulated LO for the case where the RF delay T_{RF} is present.

FIG. 3C is a graph illustrating the case FIG. 3B but with applied delay compensation.

FIG. 4 is a diagram illustrating a delay compensation component for applications in polar communication systems.

FIG. 5 is a diagram illustrating a fractional phase delay filter.

FIG. 6 is an example of Matlab code that can be utilized to generate the Lagrange filter coefficients

FIG. 7 is an example of Matlab code that can be utilized to Lagrange phase delay filtering

FIG. 8 is a flow diagram illustrating a method of generating phase information from a feedback receiver.

DETAILED DESCRIPTION

The present invention will now be described with reference to the attached drawing figures, wherein like reference numerals are used to refer to like elements throughout, and wherein the illustrated structures and devices are not necessarily drawn to scale.

FIG. 1 is a simplified diagram illustrating a communication system **100** employing polar modulation that measures phase shift with enhanced accuracy. The phase shift is measured and compensated as described below. The compensated phase measurement can be utilized for a variety of applications including, but not limited to adaptive digital pre-distortion, antenna tuner, amplifier tuner, and the like. Further, the compensated phase measurement can be utilized for applications not related to communications.

The system **100** is described primarily towards transmission, however, it is appreciated the system **100** can also be

utilized for receiving. Further, the system **100** is provided in a simplified form in order to facilitate understanding. It is appreciated that variations, such as additional or varied components are contemplated.

The communication system **100** uses amplitude modulation and phase modulation to generate an output RF signal for transmission. Phase shift(s) can be introduced to the output RF signal by portions of the communication system **100**, such as the portions used for transmission. One type of phase shift is amplitude modulation to phase modulation (AM/PM) distortion. AM/PM distortion can be introduced by a power amplifier a path of the system **100**. Phase shift(s) can be independent of amplitude modulation, such as phase variations depending on the matching of a power amplifier.

The phase shifts can be accounted for if accurately measured or detected. One technique to detect these phase shifts is to use a feedback receiver to generate feedback information. The feedback information includes phase information and amplitude information and is derived at least partially from a coupled version of the output RF signal. The feedback information can then be utilized by the communication system to compensate for the detected phase shifts and enhance signal quality.

However, differences in path delays between the coupled output signal and other signals utilized in to generate the feedback information are typically present. These delay differences, even when small, diminish the accuracy and usefulness of feedback information, specifically when using a phase modulated LO to generate the feedback phase information. For example, the feedback information may be insufficient to allow sufficient accuracy of the phase shifts measurement. As a result, a selected or desired signal quality may not be attainable.

The system **100** identifies the delay differences in path delays and compensates the feedback information from the feedback receiver by accounting for path delays. The compensated feedback information more closely or accurately represents phase shifts present in the RF output signal. Thus, the phase shifts can be measured accurately by removing or accounting for the impact of the unwanted path delay.

The system **100** includes a polar conversion component **102**, a polar modulator **103**, an RF front end **104**, a feedback receiver **106**, and a delay compensation component **108**. The polar conversion component **102** and the polar modulator **103** can be considered part of a transmission path. The system **100** is configurable to provide a modulated RF output signal to an antenna **110** and generates a compensated feedback receiver (FBR) phase information signal **112**.

The polar conversion component **102** receives an input signal and provides polar modulation components, which are provided to the polar modulator **103**. The polar modulator **103** generates a modulated RF signal that can be used for transmission. The input signal is a baseband signal that has been modulated from a data signal, in digital form. The input signal, in this example, includes in-phase (I) and quadrature-phase (Q) symbols. The symbol components are also referred to as Cartesian symbol components. As stated above, the polar conversion component **102** converts the I/Q vector modulation components into polar modulation components. The Cartesian symbol components are converted into amplitude modulation (AM) symbol components (A) and phase modulation (PM) symbol component (ϕ or P), also referred to as polar components.

The polar components are converted to analog signals by the polar modulator **103** and provided as the modulated or RF signal for transmission. A digital to analog converter can be used to convert the "A" components into an analog amplitude

modulation signal and a DPLL is used to convert the “P” components into an analog modulation signal. The analog signals are combined and provided as the modulated RF signal **122**. The polar modulator **103** also provides a portion of the phase modulated signal as a phase modulated local oscillator (LO) signal **114**. The phase modulated LO signal is a local oscillator signal modulated with the phase information of the analog phase modulation signal. The polar modulator **103** has an associated delay, referred to as a phase delay (T_{TX}).

The RF front end **104** generally amplifies and filters the modulated RF signal to facilitate transmission of the signal. The RF front end **104** provides the amplified and filtered signal as an output signal **116**, which can then be transmitted via an antenna. The RF front end **104** also provides a coupled version **118** of the output signal. The output signal has an associated propagation delay, referred to as a second RF path delay and is denoted as T_{RF2} .

The RF front end **104** can introduce phase shifts into the output signal. One type of the phase shift is AM/PM distortions, described above. The AM/PM distortions can be introduced, for example, by a power amplifier within the RF path. These phase shifts, including the AM/PM distortions, are present in the coupled version of the output signal.

The feedback receiver **106** receives the coupled version **118** of the output signal and the phase modulated local oscillator signal **114**. The phase modulated local oscillator signal also has an associated propagation delay, referred to as a first RF path delay and is denoted as T_{RF1} . The first RF path delay is the propagation time from the polar modulator **103** to the feedback receiver **106**.

The feedback receiver **106** extracts phase and magnitude information from the signal **118** using the phase modulated local oscillator signal **114** to generate feedback information. The feedback information includes FBR phase information and amplitude information. The feedback information generated by the feedback receiver **106** can facilitate or be part of a linearization mechanism to extract an error signal comprising phase shift(s), such as phase and magnitude distortion, which can be utilized to pre-distort the modulated RF signal. The feedback receiver **106**, in this example, provides phase information in the form of a feedback receiver (FBR) phase information signal **120**.

In one example, the feedback receiver **106** demodulates the coupled output signal **118** using the phase modulated local oscillator signal **114**. The demodulated signals are filtered and converted to digital signals. At least a portion of the digital signals comprise the FBR phase signal. Further, there is also a propagation delay along the path of the feedback receiver **106**, referred to as a feedback receiver path delay, which is denoted as T_{FBR} .

However, delay difference between the first RF path delay and the second RF path delay results in unwanted FBR phase signal variations and can degrade the overall signal quality dramatically. The delay difference between the first RF path delay and the second RF path delay is referred to as RF delay and denoted as T_{RF} .

The delay compensation component **108** receives the FBR phase information signal **120** and generates a compensated FBR phase information signal **112**. The compensated signal **112** provides a measurement of phase shift(s) with enhanced accuracy because the delay compensation component **108** compensates for the RF delay differences.

FIG. 2 is a diagram illustrating a more detailed communication system **200** employing polar modulation. The system **200** measures phase shift(s) with enhanced accuracy by accounting for delay differences along paths of the system **200**.

For illustrative purposes, the system **200** is described with regards to transmission. It is appreciated that suitable variations in the system **200** are contemplated. Further, it is also appreciated that other suitable applications for the compensated phase information signal are also contemplated.

The system **200** includes a CORDIC **202** that receives Cartesian symbol components including in-phase (I) and quadrature-phase (Q) symbols. The CORDIC **202**, converts the Cartesian symbol components into polar components, which comprise amplitude modulation (AM) symbol components (ADO and phase modulation (PM) symbol components (ϕ or P_{TX}).

The amplitude modulation components are provided to a digital to analog converter **204**, which generates an analog amplitude signal. The phase modulation components are provided to a DPLL **206**, which generates an analog phase signal using a local oscillator (LO) signal. The analog amplitude signal and the analog phase signal are combined by a mixer **208** to generate a modulated RF signal. The modulated RF signal is shown at (2) in FIG. 2 and is provided by:

$$V_{MIXout}(t) = A_{TX}(t - \tau_{TX}) \cos(\omega_0 t + \phi_{TX}(t - \tau_{TX}))$$

Where A_{TX} represents the analog amplitude signal

ω_0 is the carrier angular frequency

ϕ_{TX} represents the analog phase signal

τ_{TX} represents a polar modulator phase delay from node (1) to node (2).

The phase of the LO signal is described by:

$$\phi_{LO}(t) = \omega_0 t + \phi_{TX}(t - \tau_{TX})$$

A power amplifier **210** amplifies the modulated RF signal, which is then filtered by filter **212**. The power amplifier **210** introduces phase versus amplitude non-linearity and results in amplitude modulation to phase modulation (AM/PM) conversion. Thus, an output signal of the power amplifier **210** is provided by (delay of PA is considered as negligible):

$$V_{PA}(t) = A_{TX}(t - \tau_{TX}) \cos(\phi_0 t + \phi_{TX}(t - \tau_{TX}) + \phi_{RF})$$

The output of the filter **212** is an output RF signal, which can be transmitted by antenna **216**. A coupler **214** is present and obtains a coupled version of the output signal.

A low noise amplifier **218** receives the coupled output signal and provides the amplifier signal (4) to a demodulator **220**. The demodulator **220** is a quadrature demodulator and demodulates an input signal into I and Q components. The amplifier signal (4) is an input signal for the demodulator **220** and is shown as:

$$V_{DEMODOin}(t) = V_{PA}(t - \tau_{RF2}) = A_{TX}(t - \tau_{TX} - T_{RF2}) \cos(\omega_0 t - \omega_0 \tau_{RF2} \phi_{TX}(t - T_{TX} - \tau_{RF2}) + \phi_{RF})$$

Where τ_{RF2} is a second RF delay, which represents a delay from the power amplifier **210** along through the low noise amplifier **218** to (4) in FIG. 2.

The phase modulated LO signal from (2) is also provided as an input at (3) to the demodulator **220**. The phase modulated LO signal is given by:

$$\phi_{LO}(t - \tau_{RF1}) = \omega_0 t - \omega_0 \tau_{RF1} + \phi_{TX}(t - \tau_{TX} - \tau_{RF1})$$

Where τ_{RF1} is a first RF delay, which represents a delay from the mixer **208** at (2) to the demodulator **220** at (3) of FIG. 2.

The demodulator **220** using the phase modulated LO signal to demodulate the amplifier signal into the I and Q components. The I and Q components are filtered by filters **220** and converted to digital I/O signals at analog to digital converters **224**. A second CORDIC **226** converts the digital I and Q signals into polar components A_{FBR} and P_{FBR} , which represent FBR amplitude components/signals and FBR phase

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information/signals for a feedback receiver. The FBR phase information/signal is represented by:

$$\phi_{FBR1}(t) = -\omega_0 \tau_{RF} + \phi_{TX}(t - \tau - \tau_{RF}) - \phi_{TX}(t - \tau) + \phi_{RF}$$

Where delay τ_{RF} is given by:

$$\tau_{RF} = \tau_{RF2} - \tau_{RF1}$$

As the delay difference from the first RF path delay and the second RF path delay. A total or complete roundtrip delay from (1) to (5) of FIG. 2 is given by:

$$\tau = \tau_{TX} + \tau_{FBR} + \tau_{RF1}$$

A phase delay from the polar modulator to the feedback receiver LO input is represented by

$$\tau_{LOFBR} = \tau_{TX} + \tau_{RF1}$$

Thus, the total or complete roundtrip delay from (1) to (5) of FIG. 2 can also be given by:

$$\tau = \tau_{FBR} + \tau_{LOFBR}$$

The FBR phase information is summed with a compensation signal by adder 228 to provide compensated FBR phase information. The compensation signal is provided by a delay compensation component 226.

In the ideal case, the delay τ_{RF} is zero, which means that the first RF path delay is equal to the second RF path delay. This equation is shown as:

$$\tau_{RF} = \tau_{RF2} - \tau_{RF1} = 0;$$

because $\tau_{RF2} = \tau_{RF1}$

FIG. 3A is a graph 301 illustrating the FBR phase information from a feedback receiver for the ideal case with a PA having AMPM conversion where the delay τ_{RF} is zero. Here, the first RF path delay is equal to the second RF path delay such that their difference is zero. The FBR phase information is relative the amplitude component.

An x-axis yields values of the amplitude component $A_{TX}(t)$ and a y-axis provides values of the phase modulation signal $\phi_{FBR1}(t)$ from the feedback receiver in degrees. Both are from the digital domain and the comparison provides amplitude modulation/phase modulation characteristics of the power amplifier 210.

In the ideal case, the delay τ_{RF} is zero and there is ideal time alignment between $A_{FBR}(t)$ and $A_{TX}(t)$. As a result, the FBR phase information from the feedback receiver for the ideal case is given by:

$$\phi_{FBR1}(t) = \phi_{RF}$$

Line 311 provides the comparison of the amplitude component and the phase modulation signal. There is no difference between the first RF path delay and the second RF path delay. The AM/PM characteristic is stable as shown in the line 311. Thus, the signals from the feedback receiver can be utilized to facilitate signal generation.

However it is understood that in real world situations there will, necessarily, be a delay difference. These differences can lead to phase variations in the AM/PM characteristics provided by the feedback receiver.

FIG. 3B is a graph 302 illustrating the FBR phase information from a feedback receiver for the normal case where the delay is present. Here, the first RF path delay is not equal to the second RF path delay. The FBR phase information is relative the amplitude component.

An x-axis yields values of the amplitude component $A_{TX}(t)$ and a y-axis provides values of the FBR phase information $\phi_{FBR1}(t)$ from the feedback receiver in degrees. Both are from

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the digital domain and the comparison provides amplitude modulation/phase modulation characteristics of the power amplifier 210.

Here, the delay τ_{RF} is different from zero. The FBR phase information is disrupted by the phase difference of the phase modulated FBR LO and the phase of the RF signal due to RF delay. Thus, the FBR phase information is given by:

$$\phi_{RF} \text{ and it is disrupted by}$$

$$\phi_{TX}(t - \tau - \tau_{RF}) - \phi_{TX}(t - \tau)$$

Line 321 provides the comparison of the amplitude component and the FBR phase information for the normal case. The line 321 represents an example with a UMTS Rel. 99 signal having a symbol rate of 3.84 MSps and a delay τ_{RF} of 10 ns. It can be seen from line 321 that even a relatively small delay can result in a large amount of distortion or variation in the FBR phase information. This reduces signal quality dramatically.

As stated above, the system 200 adds a compensation signal to the FBR phase information/signal via the adder 228. The adder 228 provides the compensated FBR phase information. The compensated FBR phase information mitigates reduction in signal quality, such as that seen in FIG. 3B. The compensation signal is generated by the delay compensation component.

FIG. 3C is a graph 303 illustrating the compensated FBR phase information from a feedback receiver for the normal case. Here again, the first RF path delay is not equal to the second RF path delay. The FBR phase information is presented relative the amplitude component.

An x-axis yields values of the amplitude component $A_{TX}(t)$ and a y-axis provides values of the compensated FBR phase information $\phi_{FBR1}(t)$ from the feedback receiver in degrees. Both are from the digital domain and the comparison provides amplitude modulation/phase modulation characteristics of the power amplifier 210.

Here again, the delay τ_{RF} is different from zero. The FBR phase information is disrupted by the phase variations. Thus, (uncompensated) the FBR phase information is given by:

$$\phi_{RF} \text{ and it is disrupted by}$$

$$\phi_{TX}(t - \tau - \tau_{RF}) - \phi_{TX}(t - \tau)$$

The compensation signal provided by the delay compensation component 226 is obtained by:

$$\phi_{TX}(t - \tau) - \phi_{TX}(t - \tau - \tau_{RF})$$

The compensation signal is added to the FBR phase information from the FBR by the adder 226 to obtain the compensated FBR phase information signal given by:

$$\phi_{FBR}(t) = \phi_{FBR1}(t) + \phi_{TX}(t - \tau) - \phi_{TX}(t - \tau - \tau_{RF}) - \omega_0 \tau_{RF} + \phi_{RF}$$

Where $\phi_{FBR}(t)$ is the compensated FBR phase information.

The remaining term $-\omega_0 \tau_{RF}$ can be removed by calibration.

Line 331 provides a comparison of the FBR amplitude component/information and the compensated FBR phase information for the normal case. The applied compensation can be seen by comparing line 331 with line 321 of FIG. 3B. Here, the examples is similar to that used in FIG. 3B with a UMTS Rel. 99 signal having a symbol rate of 3.84 MSps and a delay τ_{RF} of 10 ns. However, signal quality is improved and similar to the ideal case shown in FIG. 3A.

As stated above, the system 200 adds a compensation signal to the FBR phase information/signal via the adder 228. The adder 228 provides the compensated FBR phase information. The compensated FBR phase information mitigates

reduction in signal quality, such as that seen in FIG. 3B. The compensation signal is generated by the delay compensation component 226.

The delay compensation component 226 obtains and analyzes the propagation delays present in the system 200 in order to generate the compensation signal. In one example, the delay compensation component 226 uses a two delay filter to generate the compensation signal. A first filter compensates for a roundtrip delay and a second filter compensates for the RF delay. Additional details of an example delay compensation component are provided below.

FIG. 4 is a diagram illustrating a delay compensation component 400 for applications in communication systems. The delay compensation component 400 facilitates generation of a compensated FBR phase information signal that enhances signal quality by compensating for delay differences in RF path propagations and path delays.

The delay compensation component 400 provides a compensation signal to an adder 402 at (5). The adder 402 corresponds to the adder 228 of FIG. 2. The adder 402 adds a FBR phase information with the compensation signal to generate the compensated FBR phase information signal.

The delay compensation component 400 includes an RF delay filter 408, a filter adder 406, and a roundtrip delay filter 404. Both filters operate in the digital domain. A phase symbol component is provided at (1), which corresponds to the similar denoted location in FIG. 2. The phase symbol component is provided to the RF delay filter 408.

The RF delay filter 408 filters the phase symbol component according to the difference between the first RF path delay and the second RF path delay, described above. The RF delay filter 408 is an integer and fractional delay filter. The filtered component is subtracted from the phase symbol component by the RF adder 406. The resulting component is provided as an input to the roundtrip delay filter 404. The resulting component is filtered according to the roundtrip delay to generate the compensation signal. The roundtrip delay filter 404 is also an integer and fractional delay filter.

FIG. 5 is a diagram illustrating a fractional phase delay filter 500. The filter 500 is provided as an example for a fractional phase delay filter, using state unwrapping for the phase discontinuity problem at $+\pi$, $-\pi$.

The filter includes a state unwrapper 504, a delay filter chain 506, chain coefficients 508, chain multipliers 510, and an adder 512. Phase jumps are detected by the unwrapper 504 and the state of the filter is corrected, to prevent the filter from numerical artifacts resulting from the $+\pi$, $-\pi$ wrap. So the whole filter behaves like a filter applied on a phase signal with an unlimited phase input range and without phase discontinuities. This filter can be of any order greater or equal to 1. Filter coefficients b_2 to b_n are the digital FIR filter coefficients of a standard fractional delay filter. Such filter coefficients can be calculated by using a suitable approach, such as the Lagrange fractional delay filter approach, shown in FIG. 6.

The filter 500 is utilized for normal operation because phase symbol components have discontinuities by wrapping it around a numeric range. The discontinuities can be handled in several ways. One way is to neglect values around discontinuities to mitigate errors by filter settling, unwrap filter states as input signal discontinuities enter the delay filter chain, or differentiate phase to frequency domain, apply delay filtering, and integrate to the phase domain to obtain the result.

FIG. 6 is an example of matlab code that can be utilized to generate the Lagrange filter coefficients b_1 and b_2 . The code

shown in FIG. 6 is one example of a suitable approach to obtain filter coefficients. It is appreciated that other suitable approaches can be utilized.

FIG. 7 is an example of matlab code that can be utilized to Lagrange phase delay filtering with two coefficients and to perform state unwrap. The code provided is an example of a suitable technique for the phase state unwrapper. It is appreciated that other suitable techniques are contemplated.

FIG. 8 is a flow diagram illustrating a method 800 of generating phase information from a feedback receiver. The phase information is obtained by considering path delays and compensating for those resulting phase variations. As a result, the phase information from the feedback receiver can be utilized to enhance transmission signal quality.

The method begins at block 802, wherein a path delay difference is obtained. The path delay difference is the difference between a path delay for a coupled output signal and a path delay for a phase modulated local oscillator signal.

A roundtrip delay is obtained at block 804. The roundtrip delay includes a polar modulator phase delay, a first RF path delay, and a feedback receiver path delay. The above description, including the description of FIG. 2, can be referenced for a description of the various delays involved.

A feedback receiver generates an FBR phase information signal from the coupled output signal and the phase modulated local oscillator signal at block 806. The feedback receiver typically generates feedback information, which includes the FBR phase information and additionally includes FBR amplitude information.

A compensation signal is generated at block 808 according to the path delay difference and the roundtrip delay to remove phase variations. A delay compensation component utilizing filters can be utilized to generate the compensation signal. In one example, phase symbol components are filtered with the delays to generate the compensation signal.

In another example, an integer and fractional delay filter is utilized to generate the compensation signal. The fractional portion can be realized, for example, by using Lagrange interpolation, an all pass filter, a sinc interpolation filter, and the like.

The compensation signal is combined with the FBR phase information at block 810 to generate a compensated FBR phase information signal. The compensation signal compensates for the phase variations present in the communication system.

While the methods provided herein are illustrated and described below as a series of acts or events, the present disclosure is not limited by the illustrated ordering of such acts or events. For example, some acts may occur in different orders and/or concurrently with other acts or events apart from those illustrated and/or described herein. In addition, not all illustrated acts are required and the waveform shapes are merely illustrative and other waveforms may vary significantly from those illustrated. Further, one or more of the acts depicted herein may be carried out in one or more separate acts or phases.

Furthermore, the claimed subject matter may be implemented as a method, apparatus, or article of manufacture using standard programming and/or engineering techniques to produce software, firmware, hardware, or any combination thereof to control a computer to implement the disclosed subject matter (e.g., the circuits shown in FIG. 2, 3, etc., are non-limiting examples of circuits that may be used to implement method(s) and/or variations thereof). The term "article of manufacture" as used herein is intended to encompass a computer program accessible from any computer-readable device, carrier, or media. Of course, those skilled in the art

will recognize many modifications may be made to this configuration without departing from the scope or spirit of the claimed subject matter.

A communication system includes a polar conversion component, a polar modulator, an RF front-end component, a feedback receiver, a delay compensation component, and an adder. The polar conversion component is configured to provide an amplitude signal and a phase signal. The polar modulator is configured to receive amplitude signal and the phase signal and to provide the phase modulated local oscillator signal and an RF output signal. The RF front-end component is configured to receive the RF output signal and to provide a coupled output signal. The feedback receiver is configured to receive the phase modulated local oscillator signal and the coupled output signal and to generate an uncompensated feedback phase information signal. The delay compensation component is configured to receive the phase signal and the uncompensated feedback phase information signal and to generate a compensation signal. The adder is configured to add the compensation signal to the uncompensated feedback phase information signal to generate a compensated feedback phase information signal.

A delay compensation component includes a first filter, an adder, and a second filter. The first filter is configured to filter a phase symbol component according to first delay elements to generate a first filter output. The adder is configured to subtract the first filter output from the phase symbol component to generate an adder output. The second filter is configured to filter the adder output according to second delay elements to generate a second filter output.

A method of operating a communication system is disclosed. A path delay difference for first and second signals is obtained. A roundtrip delay for the system is obtained. A compensation signal is generated according to the RF path delay difference and the roundtrip delay. The compensation signal is combined with the phase information signal to generate a compensated phase information signal.

Although the invention has been illustrated and described with respect to one or more implementations, alterations and/or modifications may be made to the illustrated examples without departing from the spirit and scope of the appended claims. For example, although the transmission circuit described herein has been illustrated as a transmitter circuit, one of ordinary skill in the art will appreciate that the invention provided herein may be applied to transceiver circuits as well. Furthermore, in particular regard to the various functions performed by the above described components or structures (assemblies, devices, circuits, systems, etc.), the terms (including a reference to a “means”) used to describe such components are intended to correspond, unless otherwise indicated, to any component or structure which performs the specified function of the described component (e.g., that is functionally equivalent), even though not structurally equivalent to the disclosed structure which performs the function in the herein illustrated exemplary implementations of the invention. In addition, while a particular feature of the invention may have been disclosed with respect to only one of several implementations, such feature may be combined with one or more other features of the other implementations as may be desired and advantageous for any given or particular application. Furthermore, to the extent that the terms “including”, “includes”, “having”, “has”, “with”, or variants thereof are used in either the detailed description and the claims, such terms are intended to be inclusive in a manner similar to the term “comprising”.

What is claimed is:

1. A communications system comprising:

- a polar conversion component configured to provide an amplitude signal and a phase signal;
- a polar modulator configured to receive the amplitude signal and the phase signal and to provide a phase modulated local oscillator signal and an RF output signal;
- an RF front-end component configured to receive the RF output signal and to provide a coupled output signal;
- a feedback receiver configured to receive the phase modulated local oscillator signal and the coupled output signal and to generate an uncompensated feedback phase information signal;
- a delay compensation component configured to receive the phase signal from the polar conversion component, to receive the uncompensated feedback phase information signal from the feedback receiver, to utilize an RF delay and a roundtrip delay, and to generate a compensation signal based on the uncompensated feedback phase information signal, the roundtrip delay and the RF delay, wherein the RF delay is at least partially based upon a path of the phase modulated local oscillator signal; and
- an adder configured to add the compensation signal to the uncompensated feedback phase information signal to generate a compensated feedback phase information signal.

2. The system of claim 1, wherein the RF delay is the delay between the phase modulated local oscillator signal and the phase information of the coupled output signal.

3. The system of claim 1, wherein the roundtrip delay is a combination of a first delay and a second delay, wherein the first delay is the delay between the phase modulation signal of the feedback receiver local oscillator input signal and the phase signal from the polar conversion component and the second delay is a feedback receiver path delay.

4. The system of claim 1, wherein the delay compensation component includes a first digital filter, the first digital filter being an integer and/or fractional delay filter.

5. The system of claim 4, wherein the first filter operates according to a path delay difference, the path delay difference being a difference between the first RF path delay and the second RF path delay.

6. The system of claim 4, wherein the delay compensation component further includes a second digital filter that operates according to a roundtrip delay and receives an output of the first filter as an input.

7. The system of claim 4, wherein the delay compensation component includes a second digital filter that operates according to a roundtrip delay, wherein an output of the second digital filter is provided as an input to the first digital filter.

8. The system of claim 6, wherein the delay compensation component further includes a delay adder configured to add the output of the first filter to phase symbol components and provide the sum to the second filter as the input.

9. The system of claim 1, wherein the compensated feedback phase information signal represents phase shifts present in the RF output signal.

10. The system of claim 1, wherein the feedback receiver is configured to extract phase and amplitude information from the coupled output signal using the phase modulated local oscillator signal.

11. The system of claim 10, wherein the feedback receiver is further configured to provide the extracted phase information as the uncompensated feedback phase information signal.

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12. The system of claim 1, wherein the feedback receiver is configured to demodulate the coupled output signal using the phase modulated local oscillator signal to generate the uncompensated feedback phase information signal.

13. The system of claim 1, wherein the delay compensation component is configured to generate the compensation signal based on the phase signal and the uncompensated feedback phase information signal.

14. A communications system comprising:

a polar modulator configured to receive an amplitude signal and a phase signal and generate a modulated radio-frequency (RF) signal based on the amplitude signal and the phase signal, and generate a phase modulated local oscillator (LO) signal based on the phase signal;

a feedback receiver configured to receive the phase modulated LO signal and an RF output signal based on the modulated RF signal and configured to demodulate the RF output signal using the phase modulated LO signal to generate an uncompensated feedback phase information signal;

a delay compensation component configured to generate a compensation signal based on the phase signal received at the polar modulator; and

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an adder configured to add the uncompensated feedback phase information signal and the compensation signal to form a compensated feedback phase information signal; wherein the phase modulated LO signal has a first path delay and the RF output signal has a second path delay and the feedback receiver is configured to generate the uncompensated feedback phase information signal having a delay difference between the first path delay and the second path delay.

15. The system of claim 14, wherein the uncompensated feedback phase information signal includes phase information extracted from the RF output signal.

16. The system of claim 14, wherein the feedback receiver includes a quadrature demodulator configured to demodulate the modulated RF signal using the phase modulated LO signal into quadrature components and the feedback receiver is configured to determine the delay difference based on the quadrature components.

17. The system of claim 14, wherein the feedback receiver is configured to demodulate the RF output signal to obtain demodulated signals and to convert the demodulated signals to digital signals and wherein the uncompensated feedback phase information signal includes the digital signals.

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